

1. Purpose

The purpose of this **reliability standard** is to set load-responsive protection relays associated with generation facilities at a level to prevent unnecessary tripping of a **generating unit** or an **aggregated generating facility** during a **disturbance** for conditions that do not pose a risk of damage to the associated equipment.

2. Applicability

2.1 Inclusions

This reliability standard applies to:

- (a) the **legal owner** of a **generating unit**, including all electrical equipment that connects the stator windings of any **generating unit** to the **transmission system**, that is:
 - directly connected to the **bulk electric system**, or that is part of an industrial complex that is directly connected to the **bulk electric system**, and has a **maximum authorized real power** rating greater than 18 MW;
 - (ii) within a power plant or industrial complex which:
 - (A) is not part of an aggregated generating facility;
 - (B) is directly connected to the **bulk electric system**; and
 - (C) has a combined maximum authorized real power rating greater than 67.5 MW;
 - (iii) a blackstart resource; or
 - (iv) material to this **reliability standard** and to the **reliability** of either the **interconnected electric system** or the City of Medicine Hat electric system as the **ISO** determines and publishes on the AESO website and may amend from time to time on notice to **market participants** in accordance with the process set out in Appendix 1;
- (b) the legal owner of an aggregated generating facility that is:
 - (i) directly connected to the **bulk electric system** and has a **maximum authorized real power** rating greater than 67.5 MW;
 - (ii) within a power plant or industrial complex which:
 - (A) is directly connected to the **bulk electric system**; and
 - (B) has a combined maximum authorized real power rating greater than 67.5 MW;
 - (iii) a blackstart resource; or
 - (iv) material to this reliability standard and to the reliability of either the interconnected electric system or the City of Medicine Hat electric system as the ISO determines and publishes on the AESO website and may amend from time to time on notice to market participants in accordance with the process set out in Appendix 1;
- (c) the **legal owner** of a **transmission facility** that is:
 - (i) part of the **bulk electric system**; or
 - (ii) which the **ISO** determines is necessary for the reliable operation of either the **interconnected electric system** or the City of Medicine Hat electric system and publishes on the AESO



website and may amend from time to time on notice to **market participants** in accordance with the process set out in Appendix 1.

2.2 Exclusions

This **reliability standard** does not apply to the following **protection systems**:

- (a) any protection relay elements that are in-service only during startup of a generating unit;
- (b) load-responsive components of a protection system that are armed only when the generating unit is disconnected from the interconnected electric system;
- (c) phase **fault** detector protection relay elements employed to supervise other load-responsive phase protection distance relays, provided the phase distance relay is set in accordance with the criteria outlined in this **reliability standard**;
- (d) protection relay elements that are only enabled when other protection elements fail;
- (e) protection relay elements used only for remedial action schemes;
- (f) protection systems that detect generating unit overloads that are designed to coordinate with the generating unit short time capability by using an extremely inverse characteristic set to operate no faster than 7 seconds at 218% of full-load current, and prevent operation below 115% of full-load current; and
- (g) **protection systems** that detect transformer overloads and are designed only to respond in time periods which allow real time operating personnel 10 minutes or greater to respond to overload conditions.

3. Requirements

R1 Each legal owner of a generating unit, legal owner of an aggregated generating facility, and legal owner of a transmission facility, must apply settings that are in accordance with Table 1: Relay Loadability Evaluation Criteria, on each load-response protection relay while maintaining reliable fault protection.

4. Measures

The following measures correspond to the requirements identified in section 3 of this **reliability standard**. For example, MR1 is the measure for requirement R1.

MR1 Evidence of applying protection relay settings in accordance with requirement R1 exists. Evidence may include summaries of coordination studies, calculations, setting sheets, and protection relay test reports or records of installation of settings in protection relays including references to how the requirements of Table 1 and maintaining reliable fault protection have been met, or other equivalent evidence.

It is only necessary to provide evidence that the protection relays settings do not limit loadability. PRC-025-AB-2 does not require evidence to be provided that the protection relays reliably detect all **fault** conditions and protect the applicable **system elements** from these **faults**.

5. Appendices

Appendix 1 - Amending Process for List of Facilities



Appendix 2 - Table 1 Relay Loadability Evaluation Criteria

Revision History

Date	Description
XXXX-XX-XX	Initial release.



Appendix 1

Amending Process for List of Facilities

In order to amend any list referenced in subsections 2.1(a)(iv), 2.1(b)(iv) and 2.1(c)(ii) of section 2.1, Inclusions, the **ISO** must:

- (a) upon determining that a **generating unit**, an **aggregated generating facility**, or a **transmission facility** is to be added, notify the **legal owner** in writing and determine an effective date, which must be no less than 4 full calendar quarters after the date of notice, for the **legal owner** to meet the applicable requirements;
- (b) upon determining that a **generating unit**, an **aggregated generating facility**, or a **transmission facility** is to be deleted, notify the **legal owner** in writing and determine an effective date for the **legal owner** to no longer be required to meet the applicable requirements; and
- (c) publish the amended list with effective dates on the AESO website.



Appendix 2

Summary

Technology Type	Applicability of options
Synchronous generating units , and aggregating generating facilities comprised of synchronous generating units	1a, 1b, 1c, 2a, 2b, 2c, 3, 7a, 7b, 7c, 8a, 8b, 8c, 9a, 9b, 9c, 13a, 13b, 14a, 14b, 15a, 15b, 16a, 16b
Asynchronous generating units , and aggregating generating facilities comprised of asynchronous generating units including inverter-based installations	4, 5a, 5b, 6, 10, 11, 12, 13a, 13b, 17, 18, 19



Table 1 Relay Loadability Evaluation Criteria

Table 1. Relay Lo	adability Evaluation (Criteria		
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria
Synchronous generating units, or aggregated generating facilities	Phase distance relay (e.g. 21) – directional toward the transmission system	1a	The voltage of a generating unit stator winding terminal, collector bus , corresponding to 0.95 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The impedance element must be set less than the calculated impedance derived from 115% of: (1) Real power output – 100% of the maximum authorized real power, and (2) Reactive power output – 150% of the real power value, derived from the generating unit, or aggregated generating facility nameplate apparent power rating at rated power factor.
				OR
		1b	The voltage calculated at the generating unit stator winding terminal, collector bus , corresponding to 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer (including the transformer turns ratio and impedance).	The impedance element must be set less than the calculated impedance derived from 115% of: (1) Real power output – 100% of the maximum authorized real power, and (2) Reactive power output – 150% of the real power value, derived from the generating unit, or aggregated generating facility nameplate apparent power rating at rated power factor.
				OR

Calculations using the transmission step-up transformer turns ratio must use the actual tap that is applied (i.e. in service) for transmission step-up transformers with off-load tap changers. If onload tap changers are used, the calculations must reflect the tap that results in the lowest **generating unit** stator winding terminal voltage. When the criterion specifies the use of the transmission step-up transformer's impedance, the nameplate impedance at the nominal transmission step-up turns ratio must be used.

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Table 1. Relay Loa	Loadability Evaluation Criteria					
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria		
		1c	The simulated voltage at the generating unit stator winding terminal, collector bus coincident with the highest reactive power output achieved during field-forcing in response to a 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer prior to field-forcing.	The impedance element must be set less than the calculated impedance derived from 115% of: (1) Real power output – 100% of the maximum authorized real power, and (2) Reactive power output – 100% of the maximum gross reactive power output during field-forcing as determined by simulation.		
		TI	ne same application continues on the	e next page with a different relay type		



Application	Relay Type	Option	Bus Voltage¹	Pickup Setting Criteria	
Synchronous generating units, or aggregated generating facilities	Phase overcurrent relay (e.g. 50,51) or (51V-R) – voltage- restrained	2a	Generating unit stator winding terminal or collector bus voltage corresponding to 0.95 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the maximum authorized real power, and (2) Reactive power output – 150% of the real power value, derived from the generating unit nameplate apparent power rating at rated power factor.	
				OR	
		2b	Calculated generating unit stator winding terminal or collector bus voltage corresponding to 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer (including the transformer turns ratio and impedance).	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the maximum authorized real power, and (2) Reactive power output – 150% of the real power value, derived from the generating unit nameplate apparent power rating at rated power factor.	
			OR		
	2c	2c	Simulated generating unit stator winding terminal or collector bus voltage coincident with the highest reactive power output achieved during field-forcing in response to a 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer prior to field-forcing.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of maximum authorized real power or, and (2) Reactive power output –100% of the maximum gross reactive power output during field-forcing as determined by simulation.	



Application	adability Evaluation C Relay Type	Criteria Option	Bus Voltage¹	Pickup Setting Criteria
	Phase time overcurrent relay (e.g. 51V-C) – voltage controlled (Enabled to operate as a function of voltage)	3	Generating unit stator winding terminal or collector bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	Voltage control setting must be set less than 75% of the calculated generating unit stator winding terminal or collector bus voltage.
A different application starts on the next page				



Table 1. Relay Loa	padability Evaluation Criteria						
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria			
Asynchronous generating units or aggregated generating facilities (including inverter-based installations)	Phase distance relay (e.g. 21) – directional toward the transmission system	4	Generating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The impedance element must be set less than the calculated impedance derived from 130% of the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).			
	Phase overcurrent relay (e.g. 50, 51 or 51V-R) – voltage- restrained	5a	Generating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The overcurrent element must be set greater than 130% of the calculated current derived from the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).			
		OR					
		5b	Generating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The lower tolerance of the overcurrent element tripping characteristic must not infringe upon the resource capability (including the MVAr output of the resource and any static or dynamic reactive power devices) See Figure A.			



Table 1.	Гable 1. Relay Loadability Evaluation Criteria					
Арр	olication	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria	
		Phase time overcurrent relay (e.g. 51V-C) – voltage controlled (enabled to operate as a function of voltage)	6	Generating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	Voltage control setting must be set less than 75% of the calculated generating unit bus voltage or collector bus voltage.	
	A different application starts on the next page					



Table 1. Relay Loa	adability Evaluation C	Criteria		
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria
Relays installed on generator— side ² / collector bus side of the transmission step-up	Phase distance relay (e.g. 21) – directional toward the transmission system	7a	Generating unit stator winding terminal or collector bus voltage corresponding to 0.95 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The impedance element must be set less than the calculated impedance derived from 115% of: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 150% of the aggregate generation real power value, derived from the generator nameplate apparent power rating at rated power factor.
transformers				OR
connected to synchronous generating units or aggregated generating facilities		7b	Calculated generating unit stator or collector bus winding terminal voltage corresponding to 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer (including the transformer turns ratio and impedance).	The impedance element must be set less than the calculated impedance derived from 115% of: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 150% of the aggregate generation real power value, derived from the generating unit nameplate apparent power rating at rated power factor.
				OR

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² If the relay is installed on the high-side of the transmission step-up transformer, use Option 14.



Table 1. Relay Loa	ble 1. Relay Loadability Evaluation Criteria							
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria				
		7c	Simulated generating unit stator winding or collector bus terminal voltage coincident with the highest reactive power output achieved during field-forcing in response to a 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer prior to field-forcing.	The impedance element must be set less than the calculated impedance derived from 115% of: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output –100% of the aggregate generation maximum gross reactive power output during field-forcing as determined by simulation.				
		The same application continues on the next page with a different relay type						



Table 1. Relay Loa	adability Evaluation C	Criteria					
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria			
Relays installed on generator— side ³ / collector bus side of the transmission step-up	Phase overcurrent relay (e.g. 50 or 51)	8a	Generating unit stator winding terminal or collector bus voltage corresponding to 0.95 per nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 150% of the aggregate generation real power value, derived from the generating unit nameplate apparent power rating at rated power factor.			
transformers		OR					
connected to synchronous generating units or aggregated generating facilities		8b	Calculated generating unit stator winding or collector bus terminal voltage corresponding to 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer (including the transformer turns ratio and impedance).	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 150% of the aggregate generation real power value, derived from the generating unit nameplate apparent power rating at rated power factor.			

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 $^{^{3}}$ If the relay is installed on the high-side of the transmission step-up transformer, use Option 15.



Table 1. Relay Loa	able 1. Relay Loadability Evaluation Criteria						
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria			
		8c	Simulated generating unit stator winding terminal or collector bus voltage coincident with the highest reactive power output achieved during field-forcing in response to a 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer prior to field-forcing.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output –100% of the aggregate generation maximum gross reactive power output during field-forcing as determined by simulation.			
	The same application continues on the next page with a different relay type						



Table 1. Relay Loa	adability Evaluation (Criteria				
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria		
Relays installed on generator— side ⁴ / collector bus side of the transmission step-up	Phase directional overcurrent relay (e.g. 67) – directional toward the transmission system	9a	Generating unit stator winding terminal or collector bus voltage corresponding to 0.95 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 150% of the aggregate generation real power value, derived from the generating unit nameplate apparent power rating at rated power factor.		
transformers connected to		OR				
synchronous generating units or aggregated generating facilities		9b	Calculated generating unit stator winding or collector bus terminal voltage corresponding to 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer (including the transformer turns ratio and impedance).	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 150% of the aggregate generation real power value, derived from the generator nameplate apparent power rating at rated power factor.		
				OR		

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If the relay is installed on the high-side of the transmission step-up transformer, use Option 16.



Та	Table 1. Relay Loadability Evaluation Criteria							
	Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria			
			9c	Simulated generating unit stator winding terminal or collector bus voltage coincident with the highest reactive power output achieved during field-forcing in response to a 0.85 per unit nominal voltage on the high voltage side of the transmission step-up transformer prior to field-forcing.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output –100% of the aggregate generation maximum gross reactive power output during field-forcing as determined by simulation.			
	A different application starts on the next page							



Relay Type Option Bus Voltage Pickup Setting Criteria Relays installed on generator—side / Collector bus side of the transmission step-up transformers connected to asynchronous generating facilities comprised of asynchronous generating units, including inverter-based installations Relay Type Option Bus Voltage Phase distance relay (e.g. 21) - Girectional toward the transmission step-up transformer times the turns ratio of the transmission system Option Bus Voltage Benerating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission system The same application continues on the next page with a different relay type		dability Evaluation (D . V .V 1	
	Relays installed on generator—side ⁵ / collector bus side of the transmission step-up transformers connected to asynchronous generating units or aggregated generating facilities comprised of asynchronous generating units, including inverter-based	Phase distance relay (e.g. 21) – directional toward the transmission	10	Generating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The impedance element must be set less than the calculated impedance derived from 130% of the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).

⁵ If the relay is installed on the high-side of the transmission step-up transformer, use Option 17.



Table 1. Relay Loa	idability Evaluation Criteria							
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria				
Relays installed on generator / collector bus side of the transmission step-up transformers connected to asynchronous generating units or aggregated generating facilities comprised of asynchronous generating units, including inverter-based installations		11	Generating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer for overcurrent relays installed on the low-side.	The overcurrent element must be set greater than 130% of the calculated current derived from the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).				
		Th	ne same application continues on the	next page with a different relay type				

 $^{^{6}}$ If the relay is installed on the high-side of the transmission step-up transformer, use Option 18.



			1	
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria
Relays installed on generator – side /collector ous side of the ransmission step-up ransformers connected to asynchronous generating acilities comprised of asynchronous generating acilities comprised of asynchronous generating acilities comprised of asynchronous generating anits, including a verter-based estallations	Phase directional overcurrent relay (e.g. 67) – directional toward the transmission system ⁷	12	Generating unit bus voltage corresponding to 1.0 per unit nominal voltage of the high voltage side of the transmission step-up transformer times the turns ratio of the transmission step-up transformer.	The overcurrent element must be set greater than 130% of the calculated current derived from the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).

 $^{^{7}}$ If the relay is installed on the high-side of the transmission step-up transformer, use Option 19.



Table 1. Relay Loa	Table 1. Relay Loadability Evaluation Criteria					
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria		
Generating unit or aggregated generating facilities auxiliary transformers	Phase overcurrent relay (e.g. 50 or 51) applied at the high-side terminals of the generating unit auxiliary transformer, for which operation of the relay will cause the associated generating unit to trip.	13a	1.0 per unit of the winding nominal voltage of the generating unit auxiliary transformer.	The overcurrent element must be set greater than 150% of the calculated current derived from the generating unit auxiliary transformer maximum nameplate apparent power rating.		
			OR			
		13b	Generating unit auxiliary transformer bus voltage corresponding to the measured current.	The overcurrent element must be set greater than 150% of the generating unit auxiliary transformer measured current at the maximum authorized real power of the generating unit .		
	<u> </u>		A different application starts on th	e next page		



Table 1. Relay Loa	adability Evaluation Criteria							
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria				
Relays installed on	Phase distance	14a	0.85 per unit of the line nominal	The impedance element must be set less than the				
the high side of the transmission step-	relay (e.g. 21) – directional toward		voltage at the relay location.	calculated impedance derived from 115% of: (1) Real power output – 100% of the aggregate maximum				
up transformer ⁸	the transmission			authorized real power, and				
including relays	system			(2) Reactive power output – 120% of the aggregate generation				
installed on the				real power value, derived from the generator nameplate				
remote end of the				apparent power rating at rated power factor.				
line for system				OR				
elements that		14b	Simulated line voltage at the relay	The impedance element must be set less than the				
connect any			location coincident with the highest	calculated impedance derived from 115% of:				
transmission step-			reactive power output achieved	(1) Real power output – 100% of the aggregated maximum				
up transformers to the transmission			during field-forcing in response to a 0.85 per unit of the line nominal	authorized real power, and (2) Reactive power output –100% of the aggregate generation				
system that are			voltage at the remote end of the line	maximum gross reactive power output during field-forcing as				
used to export			prior to field-forcing.	determined by simulation.				
energy from a				e next page with a different relay type				
generating unit,			•					
aggregated								
generating								
facility, or								
generating plant –								
connected to								
synchronous generators.								

⁸ If the relay is installed on the generator-side of the transmission step-up transformer, use Option 7.



Table 1. Relay Loadak	dability Evaluation Criteria					
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria		
Relays installed on the high-side of the transmission step-up transformer ⁹ , including relays installed at the remote end of the line, for system elements that connect the	Phase Instantaneous overcurrent supervisory element (e.g. 50) – associated with current- based.	15a	0.85 per unit of the line nominal voltage at the relay location	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 120% of the aggregate generation real power value, derived from the generator nameplate apparent power rating at rated power factor.		
transmission step-up	communication-			OR		
transmission step-up transformers to the transmission system that are used to export energy directly from a generating unit, generating plant or aggregating generating facilities – connected to synchronous generators.	assisted schemes where the scheme is capable of tripping for loss of communications and/or phase time overcurrent relay (e.g. 51)	15b	Simulated line voltage at the relay location coincident with the highest reactive power output achieved during field-forcing in response to a 0.85 per unit of the line nominal voltage at the remote end of the line prior to field-forcing.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output –100% of the aggregate generation maximum gross reactive power output during field-forcing as determined by simulation.		
			The same application continues on	the next page with a different relay type		

⁹ If the relay is installed on the generator-side of the transmission step-up transformer use Option 8

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Table 1. Relay Loadab	oility Evaluation Crit	teria		
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria
Relays installed on the high-side of the transmission step-up transformer 10 including relays installed at the remote end of the line for system elements that connect the transmission step-up transformers to the transmission	plays installed on the high-side of the ensmission step-up ansformer to the mote end of the line ar system elements at connect the ansmission step-up ansformers to the the high side of the line ansmission step-up ansformers to the the scheme is capable of the line ansmission step-up ansformers to the the scheme is capable of the line ansmission step-up ansformers to the the scheme is capable of the line ansmission step-up ansformers to the the scheme in the line ansmission step-up ansformers to the the scheme instantaneous overcurrent supervisory element (e.g. 67) — associated with current-based, communication-assisted schemes where the scheme is capable of the line ansmission step-up ansformer to the line ansmission overcurrent supervisory element (e.g. 67) — associated with current-based, communication-assisted schemes where the scheme is capable of the line ansmission step-up ansmission ste	16a	0.85 per unit of the line nominal voltage at the relay location	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output – 120% of the aggregate generation real power value, derived from the generator nameplate apparent power rating at rated power factor.
system that are used	communications			OR
to export energy from a power plant, generating unit or aggregated generating facility – connected to synchronous generators.	the transmission system and/or phase directional time overcurrent relay (e.g. 67) – directional toward	16b	Simulated line voltage at the relay location coincident with the highest reactive power output achieved during field-forcing in response to a 0.85 per unit of the line nominal voltage at the remote end of the line prior to field-forcing.	The overcurrent element must be set greater than 115% of the calculated current derived from: (1) Real power output – 100% of the aggregate maximum authorized real power, and (2) Reactive power output –100% of the aggregate generation maximum gross reactive power output during field-forcing as determined by simulation.

 $^{^{10}}$ If the relay is installed on the generator-side of the transmission step-up transformer, use Option 9.



A different application starts on the next page



Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria		
Relays installed on he high-side of he transmission step up ransformer 11 ncluding relays nstalled at the emote end of the ine for system elements that connect the ransmission stepup transformers to he transmission system that are used to export energy from a cower plant, asynchronous generating units or aggregated generating acility comprised of asynchronous	Phase distance relay (e.g. 21) – directional toward the transmission system	17	1.0 per unit of the line nominal voltage at the relay location	The impedance element must be set less than the calculated impedance derived from 130% of the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).		
generating units ncluding inverter- pased nstallations.	The same application continues on the next page with a different relay type					

 $^{^{11}}$ If the relay is installed on the generator-side of the transmission step-up transformer, use Option 10.



Table 1. Relay Loa	ole 1. Relay Loadability Evaluation Criteria					
Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria		
Relays installed on the high side of the transmission step-up transformer 12 including relays installed at the remote end of the line for system elements that connect the transmission step-up transformers to the transmission system that are used to export energy from a	Phase overcurrent supervisory element (e.g. 50) – associated with current-based, communication-assisted schemes where the scheme is capable of tripping for loss of communications or phase time overcurrent relay (e.g. 51)	18	1.0 per unit of the line nominal voltage at the relay location	The overcurrent element must be set greater than 130% of the calculated current derived from the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).		
power plant, asynchronous		The	same application continues on the no	ext page with a different relay type		
generating unit or aggregated generating facility comprised of asynchronous generating units including inverter- based installations.						

 $^{^{12}}$ If the relay is installed on the generator-side of the transmission step-up transformer, use Option 11.

Table 1. Relay Loadability Evaluation Criteria



Application	Relay Type	Option	Bus Voltage ¹	Pickup Setting Criteria
Relay installed on the high-side of the transmission step-up transformer 13 including relays installed at the remote end of the line for system elements that connect the transmission step-up transformers to the transmission system that are used to export	element (e.g. 67) – associated with current-based, communication- assisted schemes where the scheme is	19	1.0 per unit of the line nominal voltage.	The overcurrent element must be set greater than 130% of the calculated current derived from the maximum aggregate nameplate apparent power output at rated power factor (including the reactive power output of any static or dynamic reactive power devices).

End of Table 1

tripping for loss of

directional toward

the transmission

phase directional

time overcurrent

relay (e.g. 67)

system and/or

communications

energy from a power

plant, asynchronous

generating units or

generating facility

aggregated

comprised of

asynchronous

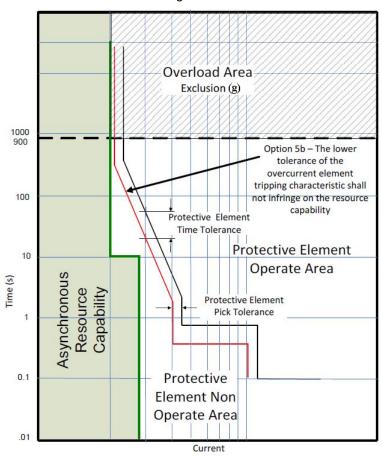
generating units

including inverterbased installations.

 $^{^{13}}$ If the relay is installed on the generator-side of the transmission step-up transformer, use Option 12.



Figure A.



This figure is for demonstration of Option 5b and does not mandate a specific type of protective curve or device manufacturer.